Table I. Rewritten alignment data

| | Alignment Details | | | | Box Design | | | | Auxiliary Circuits | | | | Impedance Peak Frequencies | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | No. | Type | $K$ | Ripple (dB) | $f_B/f_S$ | $f_H/f_S$ | $V_B/V_{AS}$ | $Q_T$ | $f_{aux}/f_S$ | $X_{aux}$ | Peak Lift (dB) | $f_{pk}/f_S$ | $f_L/f_S$ | $f_H/f_S$ | $f_H/f_L$ |
| Quasi Third Order | 1 | $QB_3$ | — | | 2.68 | 2.000 | 0.0954 | 0.180 | — | — | — | — | 0.5127 | 3.901 | 7.61 |
| | 2 | $QB_3$ | — | | 2.28 | 1.730 | 0.1337 | 0.209 | — | — | — | — | 0.5161 | 3.346 | 6.48 |
| | 3 | $QB_3$ | — | | 1.77 | 1.420 | 0.2242 | 0.259 | — | — | — | — | 0.5282 | 2.681 | 5.075 |
| | 4 | $QB_3$ | — | | 1.45 | 1.230 | 0.3390 | 0.303 | — | — | — | — | 0.5406 | 2.273 | 4.205 |
| Fourth Order | 5 | $B_4$ | 1.0 | — | 1.000 | 1.000 | 0.7072 | 0.383 | — | — | — | — | 0.5688 | 1.758 | 3.09 |
| | 6 | $C_4$ | 0.8 | — | 0.867 | 0.927 | 0.9479 | 0.415 | — | — | — | — | 0.5771 | 1.607 | 2.78 |
| | 7 | $C_4$ | 0.6 | 0.13 | 0.729 | 0.829 | 1.372 | 0.466 | — | — | — | — | 0.5741 | 1.445 | 2.52 |
| | 8 | $C_4$ | — | 0.25 | 0.641 | 0.757 | 1.790 | 0.518 | — | — | — | — | 0.5615 | 1.348 | 2.40 |
| | 9 | $C_4$ | — | 0.55 | 0.600 | 0.716 | 2.062 | 0.557 | — | — | — | — | 0.5499 | 1.302 | 2.37 |
| | 9.5 | $C_4$ | — | 1.52 | 0.520 | 0.638 | 2.60 | 0.625 | — | — | — | — | 0.5166 | 1.235 | 2.39 |
| Fifth Order | 10 | $B_5$ | 1.0 | — | 1.000 | 1.000 | 1.000 | 0.447 | 1.000 | — | — | — | 0.6180 | 1.618 | 2.62 |
| | 11 | $C_5$ | 0.7 | — | 0.852 | 0.912 | 1.715 | 0.545 | 1.218 | — | — | — | 0.6451 | 1.414 | 2.19 |
| | 12 | $C_5$ | 0.4 | 0.25 | 0.724 | 0.814 | 3.663 | 0.810 | 1.810 | — | — | — | 0.6666 | 1.221 | 1.83 |
| | 13 | $C_5$ | 0.355 | 0.5 | 0.704 | 0.798 | 4.405 | 0.924 | 2.06 | — | — | — | 0.6713 | 1.189 | 1.77 |
| | 14 | $C_5$ | 0.278 | 1.0 | 0.685 | 0.781 | 5.236 | 1.102 | 2.47 | — | — | — | 0.6725 | 1.161 | 1.73 |
| Sixth Order Class I | 15 | $B_6$ | 1.0 | — | 1.000 | 1.000 | 0.366 | 0.299 | 1.000 | 0.518 | + 6.0 | 1.070 | 0.4710 | 2.123 | 4.51 |
| | 16 | $C_6$ | 0.8 | — | 0.850 | 0.979 | 0.429 | 0.317 | 0.858 | 0.420 | + 7.7 | 0.901 | 0.4864 | 2.013 | 4.14 |
| | 17 | $C_4$ | 0.6 | — | 0.698 | 0.931 | 0.552 | 0.348 | 0.712 | 0.318 | +10.1 | 0.733 | 0.5032 | 1.850 | 3.68 |
| | 18 | $C_6$ | 0.5 | — | 0.620 | 0.888 | 0.662 | 0.371 | 0.639 | 0.265 | +11.6 | 0.651 | 0.5094 | 1.743 | 3.42 |
| | 19 | $C_6$ | 0.414 | 0.1 | 0.554 | 0.841 | 0.800 | 0.399 | 0.576 | 0.2215 | +13.2 | 0.576 | 0.5123 | 1.642 | 3.20 |
| Sixth Order Class II | 20 | $B_6$ | 1.0 | — | 1.000 | 1.000 | 1.000 | 0.408 | 1.000 | 1.414 | — | — | 0.6180 | 1.618 | 2.62 |
| | 21 | $C_6$ | 0.8 | — | 0.844 | 0.885 | 1.385 | 0.431 | 0.928 | 1.250 | + 0.2 | 1.992 | 0.6051 | 1.463 | 2.42 |
| | 22 | $C_6$ | 0.6 | — | 0.677 | 0.738 | 2.000 | 0.461 | 0.819 | 1.029 | + 1.1 | 1.181 | 0.5611 | 1.315 | 2.34 |
| | 23 | $C_6$ | 0.5 | — | 0.592 | 0.656 | 2.415 | 0.484 | 0.752 | 0.895 | + 1.9 | 0.965 | 0.5235 | 1.253 | 2.39 |
| | 24 | $C_6$ | 0.414 | 0.1 | 0.520 | 0.584 | 2.832 | 0.513 | 0.681 | 0.766 | + 3.0 | 0.806 | 0.4832 | 1.208 | 2.50 |
| | 25 | $C_6$ | 0.268 | 0.6 | 0.404 | 0.461 | 3.623 | 0.616 | 0.553 | 0.518 | + 6.0 | 0.594 | 0.4000 | 1.153 | 2.88 |
| Sixth Order Class III | 26 | $B_6$ | 1.0 | — | 1.000 | 1.000 | 1.366 | 0.518 | 1.000 | 1.931 | — | — | 0.6599 | 1.515 | 2.30 |
| | 27 | $C_6$ | 0.268 | 0.6 | 0.778 | 0.854 | 9.091 | 1.503 | 2.12 | 1.414 | — | — | 0.7605 | 1.123 | 1.48 |
| | 28 | $QB_3$ | — | — | 0.952 | 0.971 | 0.529 | 0.328 | 1.028 | — | + 6.0 | 0 | 0.5140 | 1.889 | 3.68 |